
REPORT No. 316

TABLES FOR PRESSURE OF AIR ON COMING TO REST FROM VARIOUS SPEEDS

By A. F. ZAHM and F. A. LOUDEN

Aerodynamical Laboratory, Bureau of Construction and Repair, U. S. Navy

REPORT No. 316

TABLES FOR PRESSURE OF AIR ON COMING TO REST FROM VARIOUS SPEEDS

By A. F. ZAHM and F. A. LOUDEN

In Technical Report No. 247 of the National Advisory Committee for Aeronautics theoretical formulas are given from which was computed a table for the pressure of air on coming to rest from various speeds, such as those of aircraft and propeller blades. In that report, the table gave incompressible and adiabatic stop pressures of air for even-speed intervals in miles per hour and for some even-speed intervals in knots per hour. Table II of the present report extends the above-mentioned table by including the stop pressures of air for even-speed intervals in miles per hour, feet per second, knots per hour, kilometers per hour, and meters per second. The pressure values in Table II are also more exact than the values given in the previous table.

To furnish the aeronautical engineer with ready numerical formulas for finding the pressure of air on coming to rest, Table I has been derived for the standard values specified below it. This table first presents the theoretical pressure-speed formulas and their working forms in C. G. S. units as given in N. A. C. A. Technical Report No. 247, then furnishes additional working formulas for several special units of speed.

TABLE I.—FORMULAS FOR PRESSURE OF AIR ON COMING TO REST FROM MODERATE SPEEDS
viz, for $V_0 < 1000$ mi./hr.

| | | Formulas for barometric plus impact pressure in standard atmospheres | |
|---|-------------------------|--|--|
| | | Incompressible p_1/p_0 | Adiabatic p_2/p_0 |
| General formula..... | | $p_1/p_0 = 1 + \rho_0 V_0^2 / 2p_0$ | $p_2/p_0 = [1 + (\gamma - 1) \rho_0 V_0^2 / 2\gamma p_0]^{1/\gamma - 1}$ |
| Specific working formula, $V_0 = \text{cm/s.}$ | | $p_1/p_0 = 1 + .60471 \times 10^{-8} V_0^2$ | $p_2/p_0 = (1 + 1.727735 \times 10^{-10} V_0^2)^{1.40}$ |
| Additional working formulas | $V_0 = \text{mi./hr}$ | $p_1/p_0 = 1 + 1.20841 \times 10^{-8} V_0^2$ | $p_2/p_0 = (1 + .345259 \times 10^{-8} V_0^2)^{1.40}$ |
| | $V_0 = \text{ft./s}$ | $p_1/p_0 = 1 + .56180 \times 10^{-8} V_0^2$ | $p_2/p_0 = (1 + 1.60513 \times 10^{-7} V_0^2)^{1.40}$ |
| | $V_0 = \text{knots/hr}$ | $p_1/p_0 = 1 + 1.60260 \times 10^{-8} V_0^2$ | $p_2/p_0 = (1 + .457884 \times 10^{-8} V_0^2)^{1.40}$ |
| | $V_0 = \text{km/h}$ | $p_1/p_0 = 1 + .46660 \times 10^{-8} V_0^2$ | $p_2/p_0 = (1 + 1.33313 \times 10^{-7} V_0^2)^{1.40}$ |
| | $V_0 = \text{m/s}$ | $p_1/p_0 = 1 + .60471 \times 10^{-8} V_0^2$ | $p_2/p_0 = (1 + 1.727735 \times 10^{-10} V_0^2)^{1.40}$ |

$p_0 = 1.0133 \times 10^8$ dynes/cm² = 1 std. atmo. } U. S. std. values. (See N. A. C. A. Technical Report No. 213.)
 $\rho_0 = .0012255$ g/cm³ }
 $\gamma = 1.40$
 $V_0 = \text{Air speed}$
 $p_1, p_2 = \text{Incompressible and adiabatic stop pressures above vacuo.}$

TABLE II.—PRESSURE OF AIR ON COMING TO REST FROM VARIOUS SPEEDS

[Symbols defined at bottom of table]

| Air speed miles per hour | Barometric plus impact pressure in standard atmos- pheres: 1 std. atmo. = 1.0133×10^6 dynes/cm ² = p_0 | | Impact pressure in pounds per square foot: 1 std. atmo. = 2,116.8 lb./sq. ft. | | Impact pressure in inches of water: 1 std. atmo. = 407.2 in. of water | | Percentage difference |
|--------------------------------|---|------------|---|-----------|---|-----------|--------------------------|
| | Incompressible | Adiabatic | Incompress- ible | Adiabatic | Incompress- ible | Adiabatic | |
| 0 | 1.00000000 | 1.00000000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
| 10 | 1.00012084 | 1.00012084 | .256 | .256 | .049 | .049 | .00 |
| 20 | 1.00048336 | 1.00048343 | 1.023 | 1.023 | .197 | .197 | .01 |
| 30 | 1.0010876 | 1.0010880 | 2.302 | 2.303 | .443 | .443 | .04 |
| 40 | 1.0019335 | 1.0019348 | 4.093 | 4.096 | .787 | .788 | .07 |
| 50 | 1.0030210 | 1.0030243 | 6.395 | 6.402 | 1.230 | 1.231 | .11 |
| 60 | 1.0043503 | 1.0043569 | 9.209 | 9.223 | 1.771 | 1.774 | .15 |
| 70 | 1.0059212 | 1.0059338 | 12.534 | 12.561 | 2.411 | 2.416 | .21 |
| 80 | 1.0077338 | 1.0077553 | 16.371 | 16.416 | 3.149 | 3.158 | .28 |
| 90 | 1.0097881 | 1.0098223 | 20.719 | 20.792 | 3.986 | 4.000 | .35 |
| 100 | 1.012084 | 1.012136 | 25.579 | 25.689 | 4.921 | 4.942 | .43 |
| 110 | 1.014622 | 1.014698 | 30.952 | 31.113 | 5.954 | 5.985 | .52 |
| 120 | 1.017401 | 1.017509 | 36.834 | 37.063 | 7.086 | 7.130 | .62 |
| 130 | 1.020422 | 1.020572 | 43.229 | 43.547 | 8.316 | 8.377 | .73 |
| 140 | 1.023685 | 1.023886 | 50.136 | 50.562 | 9.645 | 9.726 | .85 |
| 150 | 1.027189 | 1.027454 | 57.554 | 58.115 | 11.071 | 11.179 | .97 |
| 160 | 1.030935 | 1.031278 | 65.483 | 66.209 | 12.597 | 12.736 | 1.11 |
| 170 | 1.034923 | 1.035361 | 73.925 | 74.852 | 14.221 | 14.399 | 1.25 |
| 180 | 1.039152 | 1.039702 | 82.877 | 84.041 | 15.943 | 16.167 | 1.40 |
| 190 | 1.043624 | 1.044308 | 92.343 | 93.791 | 17.764 | 18.042 | 1.57 |
| 200 | 1.048336 | 1.049175 | 102.32 | 104.09 | 19.682 | 20.024 | 1.74 |
| 210 | 1.053291 | 1.054313 | 112.81 | 114.97 | 21.700 | 22.116 | 1.92 |
| 220 | 1.058487 | 1.059721 | 123.81 | 126.42 | 23.816 | 24.318 | 2.11 |
| 230 | 1.063925 | 1.065397 | 135.32 | 138.43 | 26.030 | 26.630 | 2.30 |
| 240 | 1.069604 | 1.071352 | 147.34 | 151.04 | 28.343 | 29.055 | 2.51 |
| 250 | 1.075526 | 1.077586 | 159.87 | 164.23 | 30.754 | 31.593 | 2.73 |
| 260 | 1.081689 | 1.084101 | 172.92 | 178.02 | 33.264 | 34.246 | 2.96 |
| 270 | 1.088093 | 1.090898 | 186.48 | 192.41 | 35.871 | 37.014 | 3.18 |
| 280 | 1.094739 | 1.097987 | 200.54 | 207.42 | 38.578 | 39.900 | 3.43 |
| 290 | 1.10163 | 1.10537 | 215.13 | 223.05 | 41.384 | 42.907 | 3.68 |
| 300 | 1.10876 | 1.11305 | 230.22 | 239.30 | 44.287 | 46.034 | 3.94 |
| 310 | 1.11613 | 1.12102 | 245.82 | 256.18 | 47.288 | 49.279 | 4.21 |
| 320 | 1.12374 | 1.12931 | 261.93 | 273.72 | 50.387 | 52.655 | 4.50 |
| 330 | 1.13160 | 1.13790 | 278.57 | 291.91 | 53.588 | 56.153 | 4.79 |
| 340 | 1.13969 | 1.14680 | 295.70 | 310.75 | 56.882 | 59.777 | 5.09 |
| 350 | 1.14803 | 1.15602 | 313.35 | 330.26 | 60.278 | 63.531 | 5.40 |
| 400 | 1.19335 | 1.20707 | 409.28 | 438.33 | 78.732 | 84.319 | 7.10 |
| 500 | 1.30210 | 1.33612 | 639.49 | 711.50 | 123.02 | 136.87 | 11.26 |
| 600 | 1.43503 | 1.50688 | 920.87 | 1,073.0 | 177.14 | 206.40 | 16.52 |
| 700 | 1.59212 | 1.72815 | 1,253.4 | 1,541.3 | 241.11 | 296.50 | 22.97 |
| 800 | 1.77338 | 2.01124 | 1,637.1 | 2,140.6 | 314.92 | 411.78 | 30.76 |
| 900 | 1.97881 | 2.37045 | 2,071.9 | 2,901.0 | 398.57 | 558.05 | 40.01 |
| 1,000 | 2.20841 | 2.82371 | 2,558.0 | 3,860.4 | 492.06 | 742.61 | 50.92 |

TABLE II.—PRESSURE OF AIR ON COMING TO REST FROM VARIOUS SPEEDS—Continued

| Air speed feet per second | Barometric plus impact pressure in standard atmos- pheres: 1 std. atmo. = 1.0133×10^6 dynes/cm ² = p_0 | | Impact pressure in pounds per square foot: 1 std. atmo. = 2,116.8 lb./sq. ft. | | Impact pressure in inches of water: 1 std. atmo. = 407.2 in. of water | | Percentage difference |
|---------------------------------|---|-------------|---|-----------|---|-----------|--------------------------|
| | Incompressible | Adiabatic | Incompress- ible | Adiabatic | Incompress- ible | Adiabatic | |
| 0 | 1.000000000 | 1.000000000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
| 10 | 1.000056180 | 1.000056180 | .119 | .119 | .023 | .023 | .00 |
| 20 | 1.00022472 | 1.00022473 | .476 | .476 | .092 | .092 | .00 |
| 30 | 1.00050562 | 1.00050570 | 1.070 | 1.070 | .206 | .206 | .02 |
| 40 | 1.00089888 | 1.00089915 | 1.903 | 1.903 | .366 | .366 | .03 |
| 50 | 1.0014045 | 1.0014052 | 2.973 | 2.975 | .572 | .572 | .05 |
| 60 | 1.0020225 | 1.0020241 | 4.281 | 4.285 | .824 | .824 | .08 |
| 70 | 1.0027528 | 1.0027556 | 5.827 | 5.833 | 1.121 | 1.122 | .10 |
| 80 | 1.0035955 | 1.0036002 | 7.611 | 7.621 | 1.464 | 1.467 | .13 |
| 90 | 1.0045506 | 1.0045582 | 9.633 | 9.649 | 1.853 | 1.856 | .17 |
| 100 | 1.0056180 | 1.0056292 | 11.892 | 11.916 | 2.288 | 2.292 | .20 |
| 110 | 1.0067978 | 1.0068142 | 14.390 | 14.424 | 2.768 | 2.775 | .24 |
| 120 | 1.0080899 | 1.0081133 | 17.125 | 17.174 | 3.294 | 3.304 | .29 |
| 130 | 1.0094944 | 1.0095267 | 20.098 | 20.166 | 3.866 | 3.879 | .34 |
| 140 | 1.011011 | 1.011055 | 23.308 | 23.401 | 4.484 | 4.502 | .40 |
| 150 | 1.012641 | 1.012697 | 26.758 | 26.877 | 5.147 | 5.170 | .44 |
| 160 | 1.014382 | 1.014456 | 30.444 | 30.600 | 5.856 | 5.886 | .51 |
| 170 | 1.016236 | 1.016330 | 34.368 | 34.567 | 6.611 | 6.650 | .58 |
| 180 | 1.018202 | 1.018322 | 38.530 | 38.784 | 7.412 | 7.461 | .66 |
| 190 | 1.020281 | 1.020428 | 42.931 | 43.242 | 8.258 | 8.318 | .72 |
| 200 | 1.022472 | 1.022653 | 47.569 | 47.952 | 9.151 | 9.224 | .81 |
| 210 | 1.024775 | 1.024995 | 52.444 | 52.909 | 10.088 | 10.178 | .89 |
| 220 | 1.027191 | 1.027456 | 57.558 | 58.119 | 11.072 | 11.180 | .97 |
| 230 | 1.029719 | 1.030036 | 62.909 | 63.580 | 12.102 | 12.231 | 1.07 |
| 240 | 1.032360 | 1.032735 | 68.500 | 69.293 | 13.177 | 13.330 | 1.16 |
| 250 | 1.035113 | 1.035555 | 74.327 | 75.263 | 14.298 | 14.478 | 1.26 |
| 260 | 1.037978 | 1.038496 | 80.392 | 81.488 | 15.465 | 15.676 | 1.36 |
| 270 | 1.040955 | 1.041556 | 86.694 | 87.966 | 16.677 | 16.922 | 1.47 |
| 280 | 1.044045 | 1.044741 | 93.234 | 94.708 | 17.935 | 18.219 | 1.58 |
| 290 | 1.047247 | 1.048049 | 100.01 | 101.71 | 19.239 | 19.566 | 1.70 |
| 300 | 1.050562 | 1.051481 | 107.03 | 108.97 | 20.589 | 20.963 | 1.82 |
| 310 | 1.053989 | 1.055037 | 114.28 | 116.50 | 21.984 | 22.411 | 1.94 |
| 320 | 1.057528 | 1.058721 | 121.78 | 124.30 | 23.425 | 23.911 | 2.07 |
| 330 | 1.061180 | 1.062528 | 129.51 | 132.36 | 24.912 | 25.461 | 2.20 |
| 340 | 1.064944 | 1.066463 | 137.47 | 140.69 | 26.445 | 27.064 | 2.34 |
| 350 | 1.068821 | 1.070529 | 145.68 | 149.30 | 28.024 | 28.719 | 2.48 |
| 360 | 1.072809 | 1.074720 | 154.12 | 158.17 | 29.648 | 30.426 | 2.62 |
| 370 | 1.076910 | 1.079045 | 162.80 | 167.32 | 31.318 | 32.187 | 2.78 |
| 380 | 1.081124 | 1.083501 | 171.72 | 176.75 | 33.034 | 34.002 | 2.93 |
| 390 | 1.085450 | 1.088089 | 180.88 | 186.47 | 34.795 | 35.870 | 3.09 |
| 400 | 1.089888 | 1.092810 | 190.27 | 196.46 | 36.602 | 37.792 | 3.25 |
| 410 | 1.094439 | 1.097665 | 199.91 | 206.74 | 38.456 | 39.769 | 3.42 |
| 420 | 1.099102 | 1.10266 | 209.78 | 217.31 | 40.354 | 41.803 | 3.59 |
| 430 | 1.10388 | 1.10779 | 219.89 | 228.17 | 42.300 | 43.892 | 3.76 |
| 440 | 1.10876 | 1.11305 | 230.22 | 239.30 | 44.287 | 46.034 | 3.94 |
| 450 | 1.11376 | 1.11846 | 240.81 | 250.76 | 46.323 | 48.237 | 4.13 |
| 460 | 1.11888 | 1.12401 | 251.65 | 262.50 | 48.408 | 50.497 | 4.32 |
| 470 | 1.12410 | 1.12970 | 262.69 | 274.55 | 50.534 | 52.814 | 4.51 |
| 480 | 1.12944 | 1.13553 | 274.00 | 286.89 | 52.708 | 55.188 | 4.70 |
| 490 | 1.13489 | 1.14151 | 285.54 | 299.55 | 54.927 | 57.623 | 4.91 |
| 500 | 1.14045 | 1.14763 | 297.30 | 312.50 | 57.191 | 60.115 | 5.11 |
| 550 | 1.16994 | 1.18051 | 359.73 | 382.10 | 69.200 | 73.504 | 6.22 |
| 600 | 1.20225 | 1.21728 | 428.12 | 459.94 | 82.356 | 88.476 | 7.43 |
| 700 | 1.27528 | 1.30342 | 582.71 | 642.28 | 112.09 | 123.55 | 10.22 |
| 800 | 1.35955 | 1.40813 | 761.10 | 863.93 | 146.41 | 166.19 | 13.51 |
| 900 | 1.45506 | 1.53392 | 963.27 | 1,130.2 | 185.30 | 217.41 | 17.33 |
| 1,000 | 1.56180 | 1.68372 | 1,189.2 | 1,447.3 | 228.76 | 278.41 | 21.70 |
| 1,100 | 1.67978 | 1.86121 | 1,439.0 | 1,823.0 | 276.81 | 350.63 | 26.69 |
| 1,200 | 1.80899 | 2.07050 | 1,712.5 | 2,266.0 | 329.42 | 435.91 | 32.33 |
| 1,300 | 1.94944 | 2.31650 | 2,009.8 | 2,786.8 | 386.61 | 536.08 | 38.66 |
| 1,400 | 2.10113 | 2.60489 | 2,330.9 | 3,397.2 | 448.38 | 653.51 | 45.75 |
| 1,500 | 2.26405 | 2.94219 | 2,675.7 | 4,111.2 | 514.72 | 790.86 | 53.65 |

TABLE II.—PRESSURE OF AIR ON COMING TO REST FROM VARIOUS SPEEDS—Continued

| Air speed knots per hour | Barometric plus impact pressure in standard atmos- pheres: 1 std. atmo. = 1.0133×10^6 dynes/cm ² = $2\frac{1}{2}$ | | Impact pressure in pounds per square foot: 1 std. atmo. = 2,116.8 lb./sq. ft. | | Impact pressure in inches of water: 1 std. atmo. = 407.2 in. of water | | Percentage difference |
|--------------------------------|--|------------|---|-----------|---|-----------|--------------------------|
| | Incompressible | Adiabatic | Incompressible | Adiabatic | Incompressible | Adiabatic | |
| 0 | 1.00000000 | 1.00000000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
| 10 | 1.00016026 | 1.00016026 | .339 | .339 | .065 | .065 | .00 |
| 20 | 1.00064104 | 1.00064117 | 1.357 | 1.357 | .261 | .261 | .02 |
| 30 | 1.0014423 | 1.0014431 | 3.053 | 3.055 | .587 | .588 | .06 |
| 40 | 1.0025642 | 1.0025665 | 5.428 | 5.433 | 1.044 | 1.045 | .09 |
| 50 | 1.0040065 | 1.0040122 | 8.481 | 8.493 | 1.631 | 1.634 | .14 |
| 60 | 1.0057694 | 1.0057814 | 12.213 | 12.238 | 2.349 | 2.354 | .21 |
| 70 | 1.0078527 | 1.0078746 | 16.623 | 16.669 | 3.198 | 3.207 | .28 |
| 80 | 1.010257 | 1.010294 | 21.712 | 21.790 | 4.177 | 4.192 | .36 |
| 90 | 1.012981 | 1.013041 | 27.478 | 27.605 | 5.286 | 5.310 | .46 |
| 100 | 1.016026 | 1.016118 | 33.924 | 34.119 | 6.526 | 6.563 | .57 |
| 110 | 1.019391 | 1.019526 | 41.047 | 41.333 | 7.896 | 7.951 | .70 |
| 120 | 1.023077 | 1.023268 | 48.849 | 49.254 | 9.397 | 9.475 | .83 |
| 130 | 1.027084 | 1.027347 | 57.331 | 57.888 | 11.029 | 11.136 | .97 |
| 140 | 1.031411 | 1.031765 | 66.491 | 67.240 | 12.791 | 12.935 | 1.13 |
| 150 | 1.036059 | 1.036524 | 76.330 | 77.314 | 14.683 | 14.873 | 1.29 |
| 160 | 1.041027 | 1.041632 | 86.846 | 88.127 | 16.706 | 16.953 | 1.47 |
| 170 | 1.046315 | 1.047087 | 98.040 | 99.674 | 18.859 | 19.174 | 1.67 |
| 180 | 1.051924 | 1.052893 | 109.91 | 111.96 | 21.143 | 21.538 | 1.87 |
| 190 | 1.057854 | 1.059060 | 122.47 | 125.02 | 23.558 | 24.049 | 2.08 |
| 200 | 1.064104 | 1.065584 | 135.70 | 138.83 | 26.103 | 26.706 | 2.31 |
| 210 | 1.070675 | 1.072478 | 149.60 | 153.42 | 28.779 | 29.513 | 2.55 |
| 220 | 1.077566 | 1.079740 | 164.13 | 168.79 | 31.585 | 32.470 | 2.80 |
| 230 | 1.084778 | 1.087375 | 179.46 | 184.96 | 34.522 | 35.579 | 3.06 |
| 240 | 1.092310 | 1.095393 | 195.40 | 201.93 | 37.589 | 38.844 | 3.34 |
| 250 | 1.10016 | 1.10380 | 212.02 | 219.72 | 40.785 | 42.267 | 3.63 |
| 260 | 1.10834 | 1.11259 | 229.33 | 238.33 | 44.116 | 45.847 | 3.92 |
| 270 | 1.11683 | 1.12179 | 247.31 | 257.81 | 47.573 | 49.593 | 4.25 |
| 280 | 1.12567 | 1.13138 | 266.02 | 278.11 | 51.173 | 53.498 | 4.57 |
| 290 | 1.13478 | 1.14139 | 285.30 | 299.29 | 54.882 | 57.574 | 4.90 |
| 300 | 1.14423 | 1.15182 | 305.31 | 321.37 | 58.730 | 61.821 | 5.26 |
| 350 | 1.19632 | 1.21047 | 415.57 | 445.52 | 79.942 | 85.703 | 7.21 |
| 400 | 1.25642 | 1.28076 | 542.79 | 594.31 | 104.41 | 114.33 | 9.49 |
| 500 | 1.40065 | 1.46130 | 848.10 | 976.48 | 163.14 | 187.84 | 15.14 |
| 600 | 1.57694 | 1.70582 | 1221.3 | 1494.1 | 234.93 | 287.41 | 22.34 |
| 700 | 1.78527 | 2.03087 | 1662.3 | 2182.1 | 319.76 | 419.77 | 31.28 |
| 800 | 2.02566 | 2.45841 | 2171.1 | 3087.2 | 417.65 | 593.86 | 42.19 |
| 900 | 2.29811 | 3.01654 | 2747.8 | 4268.6 | 528.59 | 821.14 | 55.34 |

TABLE II.—PRESSURE OF AIR ON COMING TO REST FROM VARIOUS SPEEDS—Continued

| Air speed kilometers per hour | Barometric plus impact pressure in standard atmos- pheres: 1 std. atmo. = 1.0133×10^6 dynes/cm ² = p_0 | | Impact pressure in kilograms per square meter: 1 std. atmo. = 10332 kg/m ² | | Impact pressure in millime- ters of water: 1 std. atmo. = 10343 mm of water | | Percentage difference |
|-------------------------------------|---|-------------|---|-----------|---|-----------|--------------------------|
| | Incompressible | Adiabatic | Incompres- sible | Adiabatic | Incompres- sible | Adiabatic | |
| 0 | 1.000000000 | 1.000000000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
| 10 | 1.000046660 | 1.000046660 | .482 | .482 | .483 | .483 | .00 |
| 20 | 1.00018664 | 1.00018664 | 1.928 | 1.928 | 1.930 | 1.930 | .00 |
| 30 | 1.00041994 | 1.00041999 | 4.339 | 4.339 | 4.343 | 4.344 | .01 |
| 40 | 1.00074656 | 1.00074675 | 7.713 | 7.715 | 7.722 | 7.724 | .03 |
| 50 | 1.0011665 | 1.0011670 | 12.052 | 12.057 | 12.065 | 12.070 | .04 |
| 60 | 1.0016798 | 1.0016808 | 17.356 | 17.366 | 17.374 | 17.385 | .06 |
| 70 | 1.0022863 | 1.0022882 | 23.622 | 23.642 | 23.647 | 23.667 | .08 |
| 80 | 1.0029862 | 1.0029894 | 30.853 | 30.886 | 30.886 | 30.919 | .11 |
| 90 | 1.0037795 | 1.0037843 | 39.050 | 39.099 | 39.091 | 39.141 | .13 |
| 100 | 1.0046660 | 1.0046737 | 48.209 | 48.289 | 48.260 | 48.340 | .17 |
| 110 | 1.0056459 | 1.0056573 | 58.333 | 58.451 | 58.396 | 58.513 | .20 |
| 120 | 1.0067190 | 1.0067351 | 69.421 | 69.587 | 69.495 | 69.661 | .24 |
| 130 | 1.0078855 | 1.0079077 | 81.473 | 81.702 | 81.560 | 81.789 | .28 |
| 140 | 1.0091454 | 1.0091751 | 94.490 | 94.797 | 94.591 | 94.919 | .33 |
| 150 | 1.010499 | 1.010538 | 108.48 | 108.83 | 108.59 | 108.99 | .37 |
| 160 | 1.011945 | 1.011996 | 123.42 | 123.94 | 123.55 | 124.07 | .43 |
| 170 | 1.013485 | 1.013550 | 139.33 | 140.00 | 139.48 | 140.15 | .48 |
| 180 | 1.015118 | 1.015199 | 156.20 | 157.04 | 156.37 | 157.20 | .54 |
| 190 | 1.016844 | 1.016946 | 174.03 | 175.09 | 174.22 | 175.27 | .61 |
| 200 | 1.018664 | 1.018788 | 192.84 | 194.12 | 193.04 | 194.32 | .66 |
| 210 | 1.020577 | 1.020728 | 212.60 | 214.16 | 212.83 | 221.51 | .73 |
| 220 | 1.022583 | 1.022766 | 233.33 | 235.22 | 233.58 | 235.47 | .81 |
| 230 | 1.024683 | 1.024901 | 255.02 | 257.28 | 255.30 | 257.55 | .88 |
| 240 | 1.026876 | 1.027135 | 277.68 | 280.36 | 277.98 | 280.66 | .96 |
| 250 | 1.029163 | 1.029467 | 301.31 | 304.45 | 301.63 | 304.78 | 1.04 |
| 260 | 1.031542 | 1.031899 | 325.89 | 329.58 | 326.24 | 329.93 | 1.13 |
| 270 | 1.034015 | 1.034430 | 351.44 | 355.73 | 351.82 | 356.11 | 1.22 |
| 280 | 1.036581 | 1.037062 | 377.95 | 382.92 | 378.36 | 383.33 | 1.32 |
| 290 | 1.039241 | 1.039795 | 405.44 | 411.16 | 405.87 | 411.60 | 1.41 |
| 300 | 1.041994 | 1.042627 | 433.88 | 440.42 | 434.34 | 440.89 | 1.51 |
| 310 | 1.044840 | 1.045561 | 463.29 | 470.74 | 463.78 | 471.24 | 1.61 |
| 320 | 1.047780 | 1.048599 | 493.66 | 502.12 | 494.19 | 502.66 | 1.71 |
| 330 | 1.050813 | 1.051742 | 525.00 | 534.60 | 525.56 | 535.17 | 1.83 |
| 340 | 1.053939 | 1.054986 | 557.30 | 568.12 | 557.89 | 568.72 | 1.94 |
| 350 | 1.057159 | 1.058335 | 590.57 | 602.72 | 591.20 | 603.86 | 2.06 |
| 360 | 1.060471 | 1.061787 | 624.79 | 638.38 | 625.45 | 639.06 | 2.18 |
| 370 | 1.063878 | 1.065349 | 659.99 | 675.19 | 660.69 | 675.90 | 2.30 |
| 380 | 1.067377 | 1.069012 | 696.14 | 713.03 | 696.88 | 713.79 | 2.43 |
| 390 | 1.070970 | 1.072787 | 733.26 | 752.04 | 734.04 | 752.84 | 2.56 |
| 400 | 1.074656 | 1.076667 | 771.35 | 792.12 | 772.17 | 792.97 | 2.69 |
| 410 | 1.078435 | 1.080657 | 810.39 | 833.35 | 811.25 | 834.24 | 2.83 |
| 420 | 1.082308 | 1.084754 | 850.41 | 875.68 | 851.31 | 876.61 | 2.97 |
| 430 | 1.086274 | 1.088966 | 891.38 | 919.20 | 892.33 | 920.11 | 3.12 |
| 440 | 1.090334 | 1.093284 | 933.33 | 963.81 | 934.32 | 964.84 | 3.27 |
| 450 | 1.094487 | 1.097718 | 976.24 | 1,009.6 | 977.28 | 1,010.7 | 3.42 |
| 460 | 1.098733 | 1.10226 | 1,020.1 | 1,056.6 | 1,021.2 | 1,057.7 | 3.57 |
| 470 | 1.10307 | 1.10692 | 1,064.9 | 1,104.7 | 1,066.1 | 1,105.9 | 3.74 |
| 480 | 1.10750 | 1.11169 | 1,110.7 | 1,154.0 | 1,111.9 | 1,155.2 | 3.90 |
| 490 | 1.11203 | 1.11658 | 1,157.5 | 1,204.5 | 1,158.7 | 1,205.8 | 4.06 |
| 500 | 1.11665 | 1.12159 | 1,205.2 | 1,256.3 | 1,206.5 | 1,257.6 | 4.24 |
| 510 | 1.12136 | 1.12671 | 1,253.9 | 1,309.2 | 1,255.2 | 1,310.6 | 4.41 |
| 520 | 1.12617 | 1.13196 | 1,303.6 | 1,363.4 | 1,305.0 | 1,364.9 | 4.59 |
| 530 | 1.13107 | 1.13732 | 1,354.2 | 1,418.8 | 1,355.7 | 1,467.5 | 4.77 |
| 540 | 1.13606 | 1.14280 | 1,405.8 | 1,475.4 | 1,407.3 | 1,477.0 | 4.95 |
| 550 | 1.14115 | 1.14840 | 1,458.4 | 1,533.3 | 1,459.9 | 1,534.9 | 5.14 |
| 600 | 1.16798 | 1.17830 | 1,735.6 | 1,842.2 | 1,737.4 | 1,844.2 | 6.14 |
| 700 | 1.22863 | 1.24791 | 2,362.2 | 2,561.4 | 2,364.7 | 2,564.1 | 8.43 |
| 800 | 1.29862 | 1.33184 | 3,085.3 | 3,428.6 | 3,088.6 | 3,432.2 | 11.12 |
| 900 | 1.37795 | 1.43173 | 3,905.0 | 4,460.6 | 3,909.1 | 4,465.4 | 14.23 |
| 1,000 | 1.46660 | 1.54960 | 4,820.9 | 5,678.5 | 4,826.0 | 5,684.5 | 17.79 |
| 1,100 | 1.56459 | 1.68779 | 5,833.3 | 7,106.2 | 5,839.6 | 7,113.8 | 21.82 |
| 1,200 | 1.67190 | 1.84896 | 6,942.1 | 8,771.5 | 6,949.5 | 8,780.8 | 26.35 |
| 1,300 | 1.78855 | 2.03633 | 8,147.3 | 10,707 | 8,156.0 | 10,719 | 31.42 |
| 1,400 | 1.91454 | 2.25347 | 9,449.0 | 12,951 | 9,459.1 | 12,965 | 37.06 |
| 1,500 | 2.04985 | 2.50463 | 10,847 | 15,546 | 10,859 | 15,562 | 43.32 |

TABLE II.—PRESSURE OF AIR ON COMING TO REST FROM VARIOUS SPEEDS—Continued

| Air speed meters per second | Barometric plus impact pressure in standard atmos- pheres: 1 std. atmo. = 1.0133×10^6 dynes/cm ² = p_0 | | Impact pressure in kilograms per square meter: 1 std. atmo. = 10332 kg/m ² | | Impact pressure in millime- ters of water: 1 std. atmo. = 10343 mm of water | | Percentage difference |
|-----------------------------------|---|------------|---|-----------|---|-----------|--------------------------|
| | Incompressible | Adiabatic | Incompressible | Adiabatic | Incompressible | Adiabatic | |
| 0 | 1.00000000 | 1.00000000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
| 5 | 1.00015118 | 1.00015118 | 1.562 | 1.562 | 1.571 | 1.571 | .00 |
| 10 | 1.00060471 | 1.00060482 | 6.248 | 6.249 | 6.255 | 6.256 | .02 |
| 15 | 1.0013606 | 1.0013612 | 14.058 | 14.064 | 14.073 | 14.079 | .04 |
| 20 | 1.0024188 | 1.0024209 | 24.991 | 25.013 | 25.018 | 25.039 | .09 |
| 25 | 1.0037794 | 1.0037844 | 39.049 | 39.100 | 39.090 | 39.142 | .13 |
| 30 | 1.0054424 | 1.0054531 | 56.231 | 56.341 | 56.291 | 56.401 | .20 |
| 35 | 1.0074077 | 1.0074274 | 76.536 | 76.740 | 76.618 | 76.822 | .27 |
| 40 | 1.0096754 | 1.0097089 | 99.966 | 100.31 | 100.07 | 100.42 | .35 |
| 45 | 1.012245 | 1.012299 | 126.52 | 127.07 | 126.65 | 127.21 | .44 |
| 50 | 1.015118 | 1.015199 | 156.20 | 157.04 | 156.37 | 157.20 | .54 |
| 55 | 1.018292 | 1.018412 | 188.99 | 190.23 | 189.19 | 190.44 | .66 |
| 60 | 1.021770 | 1.021989 | 224.93 | 226.67 | 225.17 | 226.92 | .78 |
| 65 | 1.025549 | 1.025783 | 263.97 | 266.39 | 264.25 | 266.67 | .92 |
| 70 | 1.029631 | 1.029946 | 306.15 | 309.40 | 306.47 | 309.78 | 1.06 |
| 75 | 1.034015 | 1.034430 | 351.44 | 355.73 | 351.82 | 356.11 | 1.22 |
| 80 | 1.038701 | 1.039241 | 399.86 | 405.44 | 400.28 | 405.87 | 1.40 |
| 85 | 1.043690 | 1.044376 | 451.41 | 458.49 | 451.89 | 458.98 | 1.57 |
| 90 | 1.048982 | 1.049845 | 506.08 | 515.00 | 506.62 | 515.55 | 1.76 |
| 95 | 1.054575 | 1.055648 | 563.87 | 574.96 | 564.47 | 575.57 | 1.97 |
| 100 | 1.060471 | 1.061787 | 624.79 | 638.38 | 625.45 | 639.06 | 2.18 |
| 105 | 1.066669 | 1.068271 | 688.82 | 705.38 | 689.56 | 706.13 | 2.40 |
| 110 | 1.073170 | 1.075103 | 755.99 | 775.96 | 756.80 | 776.79 | 2.64 |
| 115 | 1.079973 | 1.082282 | 826.28 | 850.14 | 827.16 | 851.04 | 2.89 |
| 120 | 1.087078 | 1.089818 | 899.69 | 928.00 | 900.65 | 928.99 | 3.15 |
| 125 | 1.094486 | 1.097717 | 976.23 | 1009.6 | 977.27 | 1010.7 | 3.42 |
| 130 | 1.10220 | 1.10598 | 1055.9 | 1095.0 | 1057.1 | 1096.2 | 3.70 |
| 135 | 1.11021 | 1.11461 | 1138.7 | 1184.2 | 1139.9 | 1185.4 | 3.99 |
| 140 | 1.11852 | 1.12363 | 1224.5 | 1277.3 | 1225.9 | 1278.7 | 4.31 |
| 145 | 1.12714 | 1.13302 | 1313.6 | 1374.4 | 1315.0 | 1375.8 | 4.62 |
| 150 | 1.13606 | 1.14280 | 1405.8 | 1475.4 | 1407.8 | 1477.0 | 4.95 |
| 155 | 1.14528 | 1.15298 | 1501.0 | 1580.6 | 1502.6 | 1582.3 | 5.30 |
| 160 | 1.15481 | 1.16355 | 1599.5 | 1689.8 | 1601.2 | 1691.6 | 5.65 |
| 200 | 1.24188 | 1.26351 | 2499.1 | 2722.6 | 2501.8 | 2725.5 | 8.94 |
| 250 | 1.37794 | 1.43173 | 3904.9 | 4460.6 | 3909.0 | 4465.4 | 14.23 |
| 300 | 1.54424 | 1.65842 | 5623.1 | 6802.8 | 5629.1 | 6810.0 | 20.98 |
| 350 | 1.74077 | 1.95803 | 7653.6 | 9898.4 | 7661.8 | 9908.9 | 29.33 |
| 400 | 1.96754 | 2.34964 | 9996.6 | 13944 | 10007 | 13959 | 39.49 |
| 450 | 2.22454 | 2.85774 | 12652 | 19194 | 12665 | 19215 | 51.71 |

$p_0 = 1.0133 \times 10^6$ dynes/cm² = 1 std. atmo. } U. S. std. values. (See N. A. C. A. Technical Report No. 218.)

$\rho_0 = .0012255$ g/cm³

$\gamma = 1.40$

V_0 = Air speed in cm/s.

p_1/p_0 (incompress.) = $1 + \rho_0 V_0^2 / 2p_0 = 1 + .60471 \times 10^{-6} V_0^2$ atmo.

p_1/p_0 (adiabatic) = $[1 + (\gamma - 1)\rho_0 V_0^2 / 2\gamma p_0]^{1/\gamma - 1} = (1 + 1.727735 \times 10^{-10} V_0^2)^{1.4}$

Using $\gamma = 1.404$ would lower the values in columns 6 and 7 less than 0.02 per cent for speeds less than 350 miles per hour.

AERODYNAMICAL LABORATORY,

BUREAU OF CONSTRUCTION AND REPAIR, UNITED STATES NAVY,

WASHINGTON, D. C., December 17, 1928.